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Differential axle assembly
Ausgleichsgetriebeanordnung
Ensemble d’axe différentiel

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Description

The present invention relates to work machines axles having differential gears and limited slip capability.

WO 01/111268 A1 discloses a hydraulic coupling for use in a vehicle drivetrain including a housing and a pair of rotary members projecting therefrom. A hydraulic pump is operatively supported within the housing and located within the path of the hydraulic circuit between the low-pressure and high-pressure portion.

US 3913414 A discloses an axle assembly in accordance with the preamble of claim 1.

Over the years, work machines, particularly those that operate off highway, require a differential drive mechanism for sets of wheels to accommodate vehicle turning, but, in addition, require a limited slip feature so that torque may be transferred from a slipping wheel to one that can obtain better traction. This has evolved design efforts to the point where axles can accommodate significant torque levels and, at the same time, deal with variable traction on one or the other of the drive wheels.

Design efforts have taken place that minimizes windage losses in axle assemblies where a portion, or all, of the differential gears are immersed in a lubricating liquid. As a result of the improvements in reducing windage losses, the ability to cool and lubricate various components in the differential gear assembly is challenged. Specifically, the ability to provide adequate lubrication for all of the gears is constrained by the need for reducing windage losses.

Accordingly, a need exists for an axle assembly with a differential feature that provides adequate lubrication of the components while, at the same time, reducing windage losses of the axle set.

It is therefore the object of the present invention to comply with one or all of these needs.

This object is met according to the invention by the teaching of claim 1, while features developing the solution in an advantageous manner are set forth in the further claims.

In one form, the invention is a power train axle assembly including an elongated housing and first and second shafts journaled in the elongated housing for providing a rotary output shaft at the outer ends thereof. A differential gear housing is rotatably positioned within the elongated housing and receives the inner ends of the first and second shafts. A ring gear is fixed to the differential gear housing for receiving a rotary power input. A differential gear set is positioned within the differential gear set housing and has opposed gears fixed to the inner ends of the first and second shaft and are journaled relative to the differential gear set housing. A plurality of planetary gears is journaled within the differential gear housing and mesh with the opposed gears for providing a differential action. A fluid pressure actuated differential lock mechanism has one portion thereof fixed to the differential gear housing and the other to one of the opposed gears. A source of selective fluid pressure is fluidly connected to the differential lock mechanism and provides high and low pressure levels to selectively lock the differential gear housing and one of the gears. The differential gear housing has a bleed flow path to provide pressurized fluid flow into the differential gear housing irrespective of the pressure level with the differential gear housing having a controlled seal so that fluid passes inward and out to lubricate the gears.

The above-mentioned and other features and advantages of this invention, and the manner of attaining them, will become more apparent and the invention will be better understood by reference to the following description of an embodiment of the invention taken in conjunction with the accompanying drawings, wherein:

Fig. 1 is a longitudinal section view of a work machine and an axle assembly embodying the present invention along with schematic illustrations of interconnections to additional components of the work machine;

Fig. 2 is an expanded view of a portion of the axle assembly of Fig. 1 showing a lubricant flow path.

Corresponding reference characters indicate corresponding parts throughout the several views. The exemplifications set out herein illustrate one embodiment of the invention and such exemplifications are not to be construed as limiting the scope of the invention in any manner.

Referring now to the drawings, and more particularly to Fig. 1, there is shown a work machine 10, which includes a frame and a prime mover 12 mounted in the frame, usually in the form of a compression ignition, or diesel engine, 12, which is mechanically interconnect-ed by a shaft 14 to an appropriate transmission 16 and through mechanical connection 18 to an axle assembly generally indicated by reference character 20. Axle assembly 20 includes left and right elongated housings 22 and 24 respectively mounted from a central housing 26. Elongated housings 22 and 24 provide a journal support for shafts 28 and 30 extending to wheels 32 and 34 respectively. It should be apparent to those skilled in the art that the shafts 28 and 30 may be connected to the respective wheels through reduction gear sets in order to provide the torque requirements demanded of heavy duty work machines. The central housing 26 is generally annular in form, is appropriately suspended from work machine 10, and provides a mounting for housings 22 through flange 38 by screws 36 and through flange 40 or housing 24 also by screws 36. The outer ends of shafts 28 and 30 are connected to the wheels 32 and 34 respectively and the inner ends 42 and 44 extend into a differential gear housing 46 positioned within central housing 26.

Differential gear housing 46 has first and second annular housings 48 and 50 interconnected at about the center line thereof. As described below, annular housings 48 and 50 have a substantially sealed outer...
periphery so as to retain any liquid introduced to the interior thereof within the differential gear housing 46. Housings 48 and 50 are journaled for rotation within the elongated housing 20 by bearing assemblies 52 and 54 respectively, ultimately fixed to the central housing 26. The differential gearing housing half 48 has affixed to it a ring gear 56 by screws 58. Ring gear 56 intermeshes with an unseen input pinion gear receiving input from mechanical interconnection 18. A pair of opposed end gears 62 and 64 are splined to and fixed to the inner ends of shafts 42 and 44 and are positioned within the differential gear housing 46. [0013] As shown herein, end gear 62 and 64 are bevel gears and intermesh with bevel planetary gears 66 and 68 journaled within a differential gear housing 46. As such, the input from prime mover 12 through ring gear 56 to differential gear housing 46 is transmitted to shafts 28 and 30 through planetary gears 66 and 68. As a result, the differential load on the wheels is accommodated through the differential action of the planetary gear set 66 and 68 in a manner that is well-known and understood. [0014] Because work machine 10 is heavy duty and frequently used off road where there is a difference in traction between wheels 32 and 34, a differential lock mechanism 70 is provided that selectively interconnects one of the shafts (in this case, shaft 28) to the differential gear housing 46 so as to transfer load between the shafts 28 and 30. Differential lock mechanism 70 comprises an interdigitated series of annular plates 72 and 74 received within chamber 76 in housing 48 (see Fig. 2). The annular plates 72 and 74 each have tabs 78 and 80 respectively received within slots 82 and 84 in the housing 48 and end gear 62 respectively. Plates 72 and 74 are actuated on by an annular piston assembly 86 also received within chamber 76 and abutting an axial end face of one of the annular interdigitated plates 72. To the left of piston assembly 86, as shown in Fig. 2, there is a chamber 88 fluidly connected via primary passage 90 and 92 extending through housing 48 to passages 94 in housing 50 and ultimately to a connector 96 fixed to central housing 20. The interconnection between the passages 92 and 94 and fitting 96 permits transmission of pressure when there is relative rotation between the differential gear housing 46 and central housing 20. [0015] Pressure fitting 96 connects with an appropriate line 98 to a controller 100 directing pressurized flow from a pressurized flow source 102 through passages 98, fitting 96, passages 94 and 92 to chamber 88. As illustrated herein, the fluid pressurized by system 102 is lubricant used to both reduce friction between the adjacent relatively rotating bearing parts and to provide a cooling function for the multi plate differential lock. The control system 100 uses appropriate control logic to apply the differential lock mechanism 70 as-needed to transfer torque from one axle to the other in conditions in which one of the two wheels has reduced traction. [0016] The differential axle assembly 20 is of a type that has efficient utilization of lubricant flow in order to reduce windage losses caused by gears rotating through liquid lubricant. In a standard differential housing arrangement, the housing for the opposed gears and planetary gears is significantly porous so that the differential gear set, when rotating, splashes through the liquid level within a chamber to lubricate the planetary and opposed gears. However, with efficient utilization of lubricant, there is insufficient liquid level to provide splash lubrication of the differential gear set including the differential lock assembly so as to meet the required heavy duty functions under extreme conditions. [0017] In accordance with the present invention, the differential gear housing 46 is provided with means for providing adequate lubricant and cooling functions from the liquid, while at the same time enabling efficient overall lubricant utilization. This function is shown particularly in Fig. 2 in which the primary flow path 90 to chamber 88 has a bleed flow path 104 extending from inlet passage 90 to the opposite side of annular piston 86 and into the interdigitated set of discs 72 and 74. The control system 100 directs a pressure supply from pressure source 102 of approximately 20 bar (300 psi) during engagement of the differential lock mechanism 70 but, in addition, provides a flow of a pressure level of between approximately 1-1.4 bar (15-20 psi) during disengagement of the differential lock mechanism 70 so as to provide a continuous flow of lubricant through passage 104 through the interdigitated discs 72 and 74. Furthermore, unlike previous differential gear housings, this differential gear housing 46 has the outer periphery substantially sealed so that the liquid lubricant flowing in through bleed passage 104 is maintained at a level within differential gear housing 46 that provides lubrication of the differential gear set, namely, the end gears 62, 64, and planetary gears 66 and 68. The liquid lubricant flows from the differential gear housing 46 past gear splines and bearings adjacent the centerline into the interior of housings 22, 24 and 26. When the differential lock mechanism 70 is actuated, the higher pressure flows into the disc set 72 and 74 to provide cooling thereof on account of the additional frictional forces. [0018] The above arrangement allows for a significant improvement in the efficiency and effectiveness of the axle assembly 20 in that windage losses within the central housing 26 are minimized but, at the same time, adequate liquid coolant level is maintained within differential gear housing 46 to lubricate and cool the gear set and bearings, even under the most extreme conditions encountered in an off road heavy duty work machine.

Claims

1. An axle assembly (20) for a power train, said axle assembly (20) comprising:

an housing (22, 24, 26);
first and second shafts (28, 30) journaled in said
housing (22, 24, 26) for providing a rotary output; a differential gear housing (46) rotatably positioned within said housing (22, 24, 26) and receiving inner ends (42, 44) of said first and second shafts (28, 30); a ring gear (56) fixed to said differential gear housing (46) for receiving a rotary power input; a differential gear set (66, 68) positioned within said differential gear housing (46) and having opposed gears (62, 64) fixed to the inner ends (42, 44) of said shafts (28, 30) and journaled relative to said differential gear housing (46) and a plurality of planetary gears (66, 68) journaled within said differential gear housing (46) and meshing with the opposed gears (62, 64) for providing a differential action; a fluid pressure actuated differential lock mechanism (70) having one portion (72) thereof fixed to said differential gear housing (46) and the other portion (74) thereof to one of said opposed gears (62, 64); a source (102) of selected fluid pressure fluidly connected to said differential lock mechanism (70) and providing high and low fluid pressure inputs to selectively lock and unlock said differential gear housing (46) and one of said opposed gears (62, 64); said differential gear housing (46) having a first and a second annular housing (48, 50) interconnected at about a center line thereof, the annular housings (48, 50) having a substantially sealed outer periphery so as to retain any fluid introduced into the interior thereof characterized in that said differential gear housing (46) has a bleed flow path (104) to provide pressurized fluid flow into said differential gear housing (46) irrespective of the pressure level from said source (102) of fluid pressure.

2. The axle assembly (20) according to claim 1, wherein the differential lock mechanism (70) comprises interdigitated annular plates (72, 74) and a piston (86) received within said differential gear housing (46), said piston (86) being pressurized on one side thereof to abut said plates (72, 74) in an axial direction.

3. The axle assembly (20) according to claim 2, in which the primary pressure extends to said piston (86) and the bleed flow path (104) extends from said primary flow passage (90, 92) to the interdigitated annular plates (72, 74).

4. The axle assembly (20) according to one of the claims 1 to 3, wherein the low pressure is approximately 1-1.4 bar (15-20 psi) and the high pressure is approximately 20 bar (300 psi).
ferenzialwirkung zu erzielen;
en einen mittels Fluiddruck betätigen Differenzial-
sparmehanismus (70), wobei ein Abschnitt (72) davon am Differenzialgetriebegehäuse (46) und der andere Abschnitt (74) davon an ei-
nem der gegenüberliegenden Zahnrad (62, 64) befestigt ist;
eine Quelle (102) mit ausgewähltem Fluiddruck,
die fluidisch mit dem Differenzialspermeha-
nismus (70) verbunden ist und hohe und nied-
- rigig Fluiddruckeingänge bereitstellt, um das Dif-
ferenzialgetriebegehäuse (46) sowie eines der
gegenüberliegenden Zahnräder (62, 64) wahl-
weise zu sperren und zu entsperren,
dadurch gekennzeichnet, dass
das Differenzialgetriebegehäuse (46) ein erstes
und ein zweites ringförmiges Gehäuse (48, 50)
hat, die in etwa an einer Mittellinie davon mit-
einander verbunden sind, wobei die ringförmi-
gen Gehäuse (48, 50) einen im Wesentlichen
abgedichteten Außenumfang haben, um in das
innere davon eingeleitetes Fluid zurückzuhal-
ten,
wobei das Differenzialgetriebegehäuse (46) ei-
nen Bypassströmungsweg (104) hat, um, unab-
hängig vom Druckniveau aus der für Fluiddruck
vorgesehenen Quelle (102), für eine druckbe-
aufschlagte Fluidströmung in das Differenzial-
gtriebegehäuse (46) zu sorgen.

2. Achsaggregat (20) nach Anspruch 1, bei dem der
Differenzialspermehanismus (70) ineinandergre-
fende ringförmige Platten (72, 74) sowie einen in-
nerhalb des Differenzialgetriebegehäuses (46) vorg-
gesehenen Kolben (86) umfasst, wobei der Kolben
(86) auf einer Seite davon druckbeaufschlagt ist, um
einer axialen Richtung an die Platten (72, 74) an-
zugrenzen.

3. Achsaggregat (20) nach Anspruch 1 oder 2, bei dem
der Primärströmungsdurchgang bis zum Kolben (86)
ansteht und sich der Bypassströmungsweg (104)
vom Primärströmungsdurchgang (90, 92) zu den in-
einandergreifenden ringförmigen Platten (72, 74) er-
streckt.

4. Achsaggregat (20) nach einem der Ansprüche 1 bis
3, bei dem der niedrige Druck etwa 1 - 1,4 bar (15 -
20 psi) und der hohe Druck etwa 20 bar (300 psi)
beträgt.

5. Achsaggregat (20) nach einem der Ansprüche 1 bis
4, bei dem das Differenzialgetriebegehäuse (46)
ingrömig und an den äußeren Abschnitten davon
im Wesentlichen geschlossen und abgedichtet ist,
un Fluidströmung im Inneren hin zum Zentrum des
Differenzialgetriebegehäuses (46) zu leiten.

6. Achsaggregat (20) nach einem der Ansprüche 1 bis
5, bei dem es sich bei dem Differenzialzahnradneu-
satz (66, 68) und den gegenüberliegenden Zahnraden
(62, 64) um Kegelräder handelt.

7. Achsaggregat (20) nach einem der Ansprüche 1 bis
6, bei dem die ineinandergreifenden ringförmigen
Platten (72, 74) Nasen (78, 80) haben, die in Schlitze
(82, 84) auf der Innenseite des Differenzialgetriebe-
gehäuses (46) und auf der Außenseite des eines
gegenüberliegenden Zahnrad (62, 64) eingreifen.

8. Achsaggregat (20) nach einem der Ansprüche 1 bis
7, das weiterhin einen Regler (100) umfasst, um Flui-
id mit hohem und niedrigem Druck zum Differenzi-
alspermehanismus (70) zu leiten.

9. Achsaggregat (20) nach Anspruch 8, bei dem der
Regler (100) den Druck auf einer Seite des Kolbens
(86) zwischen dem niedrigen und hohen Druck wahl-
weise regelt.

10. Achsaggregat (20) nach einem der Ansprüche 1 bis
9, bei dem das Fluid ein flüssiges Schmiermittel ist.

Revendications

1. Ensemble essieu (20) pour un groupe motopropul-
seur, ledit ensemble essieu (20) comprenant :
un boitier (22, 24, 26) ;
des premier et second arbres (28, 30) tourillon-
- nés dans ledit boitier (22, 24, 26) pour fournir
une puissance rotative en sortie ;
un boitier de différentiel (46) positionné à rota-
tion à l’intérieur dudit boitier (22, 24, 26) et re-
cevant des extrémités intérieures (42, 44) des-
dits premier et second arbres (28, 30) ;
eine couronne (56) fixée audit boitier de diffé-
rentiel (46) afin de recevoir une puissance rota-
tive en entrée ;
un train de roues dentées de différentiel (66, 68)
positionné à l’intérieur dudit boitier de diffé-
rentiel (46) et comportant des roues dentées oppo-
sées (62, 64) fixées aux extrémités intérieures
(42, 44) desdits arbres (28, 30) et
tourillonnées par rapport audit boitier de diffé-
rentiel (46) et une pluralité de satellites (66, 68)
tourillonnés à l’intérieur dudit boitier de diffé-
rentiel (46) et s’engrenant avec les roues dentées
opposées (62, 64) afin de produire un effet de diffé-
rentiel ;
um mécanisme de blocage de différentiel (70)
actionné par pression de fluide dont une partie
(72) est fixée audit boitier de différentiel (46) et
l’autre partie (74) à l’une desdites roues dentées
opposées (62, 64) ;
une source (102) de pression de fluide sélectivement raccordée, de manière à assurer une communication fluidique, audit mécanisme de blocage de différentiel (70) et fournissant des pressions de fluide en entrée élevée et basse de façon à bloquer et débloquer sélectivement ledit boîtier de différentiel (46) et l’une des dites roues dentées opposées (62, 64) ;

ledit boîtier de différentiel (46) comprenant des premier et second boîtiers annulaires (48, 50) raccordés l’un à l’autre approximativement au niveau d’une ligne médiane de ceux-ci, les boîtiers annulaires (48, 50) comportant une périphérie extérieure essentiellement hermétique de manière à retenir tout fluide introduit à l’intérieur de ceux-ci ;

**caractérisé en ce que**

ledit boîtier de différentiel (46) comporte un canal de soutirage (104) pour fournir un écoulement de fluide sous pression dans ledit boîtier de différentiel (46) quel que soit le niveau de pression provenant de ladite source (102) de pression de fluide.

2. Ensemble essieu (20) selon la revendication 1, dans lequel le mécanisme de blocage de différentiel (70) comprend des plateaux annulaires interdigités (72, 74) et un piston (86) reçus à l’intérieur dudit boîtier de différentiel (46), ledit piston (86) étant soumis à une pression sur un de ses côtés de telle sorte qu’il vienne en appui contre lesdits plateaux (72, 74) dans une direction axiale.

3. Ensemble essieu (20) selon la revendication 1 ou 2, dans lequel le passage principal s’étend jusqu’au piston (86) et le canal de soutirage (104) s’étend dudit passage principal (90, 92) aux plateaux annulaires interdigités (72, 74).

4. Ensemble essieu (20) selon l’une des revendications 1 à 3, dans lequel la pression basse est d’environ 1 à 1,4 bar (15 à 20 psi) et la pression élevée est d’environ 20 bar (300 psi).

5. Ensemble essieu (20) selon l’une des revendications 1 à 4, dans lequel le boîtier de différentiel (46) est annulaire et est essentiellement fermé et hermétique sur ses parties extérieures afin de diriger l’écoulement de fluide vers l’intérieur en direction du centre dudit boîtier de différentiel (46).

6. Ensemble essieu (20) selon l’une des revendications 1 à 5, dans lequel le train de roues dentées de différentiel (66, 68) et les roues dentées opposées (62, 64) sont des roues dentées coniques.

7. Ensemble essieu (20) selon l’une des revendications 1 à 6, dans lequel lesdits plateaux annulaires inter-
REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description