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Steam cooled gas turbine with a sliding setpoint for the high pressure bypass
Dampfgewühlte Gasturbine mit einem gleitenden Sollwert für den Hochdruckbypass
Turbine à gaz refroidie par vapeur avec une valeur de consigne glissante pour le dispositif de dérivation haute pression

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References cited:
EP-A- 0 400 370

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Description

[0001] The present invention is generally related to controlling drum pressure in a Heat Recovery Steam Generator (HRSG) that is contained in a steam cooled advanced machine gas turbine and its associated steam turbine for power generation.

[0002] In the 9H or 7H advanced machine gas turbines manufactured by General Electric, mainly steam cooling instead of air-cooling is utilized. During start-up, a sufficient flow of steam through high pressure (HP) and intermediate pressure (IP) bypass valves must be established as a permissive or threshold to cool the gas turbine before the gas turbine can be loaded beyond a minimum load. This minimum load is referred to as spinning reserve. Prior to and during spinning reserve, the gas turbine is air-cooled and must then be steam-cooled to be loaded above the spinning reserve.


[0004] In most applications, the HRSG includes three pressures of steam generation and hence three separate steam drums, high pressure steam (HP), intermediate pressure steam (IP) and low pressure steam (LP). The permissive of steam flow is established through HP and/or IP bypass valves, before the gas turbine can be steam-cooled. In order to establish the permissive of steam flow, drum pressure for the HP drum in the gas turbine must be greater than a predetermined level (i.e., a floor pressure setpoint (e.g. 49.6 bar (720 psi))). Thus, when the bypass valves are open, HP drum pressure is maintained at the floor pressure setpoint. Floor pressure is the minimum pressure at which steam may be admitted to the steam turbine.

[0005] During a cold start-up in which the advanced machine has been off for a significant time period, HP drum pressure is low due to the HRSG connected to the gas turbine being cold and the HP drum pressure being below the floor pressure setpoint. For example, during start-up of the advanced machine, the HRSG is purged by air flowing from the unfired gas turbine through the HRSG. The gas turbine is then fired (after the HRSG purge) and loaded to spinning reserve, which allows the HP drum pressure to increase due to heated flue gas entering HRSG. Eventually, the HP drum pressure is greater than the floor pressure setpoint, and the HP bypass valves open to maintain floor pressure until the gas turbine is being on steam cooled and the bypass valves close.

[0006] When the HP drum pressure is greater than the floor pressure setpoint during start-up (e.g., during start-up after a recent shutdown), the bypass valves open until floor pressure is reached and then close to maintain pressure, for example, when the gas turbine is unfired or recently fired. Therefore, energy contained in the HP drum as steam pressure is lost as steam flows through the bypass valves, prior to the gas turbine reaching spinning reserve. Accordingly, HP drum pressure must then be re-established for providing steam after spinning reserve. Therefore, time and fuel are lost as sufficient heat in the HRSG is generated and pressure in the HP drum is increased to allow the gas turbine to be loaded beyond the spinning reserve.

[0007] Consequently, a need exists for providing a technique that prevents depressurization of a HP drum in the HRSG when HP drum pressure is above a floor pressure setpoint during start-up of the advanced machine.

[0008] In one example of the invention, a bypass valve pressure setpoint, hereinafter referred to as pressure set-point, is set when an HP drum in a gas turbine is at its lowest energy level (i.e., lowest drum pressure) and still above a floor pressure setpoint. During this scenario, the HP drum pressure decays during an initial HRSG purge and increases after the gas turbine is fired. The HP drum pressure is measured and the pressure setpoint is set equal to the lowest HP drum pressure above the floor pressure setpoint. Therefore, the set pressure setpoint is greater than the floor pressure setpoint, thereby maintaining the energy contained in the HP drum. Furthermore, significant time can be saved, because HP drum pressure does not have to be re-established.

[0009] The invention will now be described in greater detail, by way of example, with reference to the drawings, in which:-

Fig. 1 illustrates an illustrative system employing the principles of the present invention; and

Fig. 2 illustrates a flow-diagram of a method according to an illustrative embodiment of the present invention.

[0010] Fig. 1 illustrates an exemplary embodiment of a power system including an advanced machine employing the principles of the present invention. An advanced machine including a gas turbine 110, which is connected to HRSG 120, generates shaft power for generator 130 includes gas turbine 110. The advanced machine is not limited to a gas turbine. One of ordinary skill in the art would readily recognize that an advanced machine may include multiple gas generators, HRSG’s, steam turbines and the like depending on the supported load.

[0011] HRSG 120 generates steam, some of which is used to cool gas turbine 110, and is coupled to gas turbine 110 via HP and/or IP bypass valves 125. The majority of the steam generated by the HRSG 120 plus the gas turbine cooling steam flows to a steam turbine 115 for power generation. Also, HRSG 120 includes high pressure (HP) drum 135 to establish the water level for an evaporator therein and to maintain pressure. The evaporator is a heat exchange surface that generates steam. Although only an HP drum 135 is shown as part of the HRSG 120 depicted in Fig. 1, it is not so limited. It should be understood that the HRSG 120 may include three pressures of steam generation and hence three separate steam
drums, High Pressure Steam (HP), Intermediate Pressure Steam (IP), and Low Pressure Steam (LP). Also, the steam turbine 115 receives boiler feed water and can emit exhaust steam to the balance of the plant 150 of the power system, and can provide shaft power to the generator 130.

[0012] During start-up, gas turbine 110 begins a start-up procedure, which includes purging of HRSG 120 with fresh air moved by a compressor of gas turbine 110 and then firing and loading of gas turbine 110 to generate power.

[0013] During the start-up procedure in a hot restart for gas turbine 110 in the advanced machine, HRSG 120 is purged by air flowing from unfired gas turbine 110 to HRSG 120. The air-flow cools steam generation and heating surfaces of HRSG 120 and lowers the pressure of HP drum 135. A hot restart corresponds to a start-up scenario in which the pressure of HP drum 135 is above the floor pressure setpoint. Typically, in a hot restart, the drum pressure was recently (e.g., the advanced machine was turned off in the last several minutes) at a high operating pressure and bypass valves 125 were closed to maintain that pressure. Fresh air from the unfired gas turbine 110 cools the HRSG 120 and evaporator water causing the pressure and the water temperature to decline. Then gas turbine 110 is fired and begins to load to a spinning reserve, and the pressure of HP drum 135 increases. At some point after the gas turbine 110 is fired, HP and/or IP bypass valves 125 open when the pressure of HP drum 135 is greater than a pressure setpoint. The pressure setpoint becomes the point at which the HP drum 135 reaches its lowest pressure during a hot restart or similar start where the drum pressure is above the preset floor pressure; otherwise, the floor pressure setpoint is used.

[0014] The pressure setpoint is a pressure value for the HP drum 135. The pressure value is based on a pressure of HP drum 135, measured during start-up, and a predetermined floor pressure setpoint for gas turbine 110. The floor pressure setpoint is a threshold that is usually determined by a manufacturer of the steam turbine 115. The steam turbine 115 accepts the steam generated in HRSG 120 and also all the cooling steam from gas turbine 110. The steam is used to generate power in the steam turbine 115. This method of setting the HP drum pressure is advantageous since the pressure being maintained allows the HP bypass valve 125 to open sooner than if, for example, the floor pressure was the setpoint, and therefore establishes steam flow. The method for setting the floor pressure setpoint is described in detail below.

[0015] The steps illustrated in Fig. 2 may be incorporated in software (e.g., firmware) running on processor-based control system 140 that is connected to and controls gas turbine 110, steam turbine 115, HRSG 120, and the balance of the plant 150. For example, control system 140 can include software for receiving measurements of HP drum pressure, setting the pressure setpoint and controlling HP and/or IP bypass valves 125, according to the method described below and shown in Fig. 2. Instituting software for controlling power generation systems is well known in the art, and one of ordinary skill in the art could readily program the steps illustrated in Fig. 2 using known programming languages and techniques.

[0016] Fig. 2 illustrates a flow-diagram of a method for setting a pressure in HP drum 135 in HRSG 120 according to a preferred embodiment of the present invention. The method illustrated in Fig. 2 is described in conjunction with an advanced machine having a gas turbine 110 shown in Fig. 1, for illustrative purposes. It should be understood that the method shown in Fig. 2 is applicable to the operation of many types of combined cycle units such as the H System™ (e.g., the 7H or 9H advanced machine gas turbine) manufactured by General Electric.

[0017] In step 200, the gas turbine 110 of the advanced machine begins a start-up procedure. Next, in step 205, the pressure of HP drum 135 is measured and a new pressure value (NP) is read continuously, on the order of once every 1/8 of a second. The time period between successive pressure measurements of HP drum 135 is readily determined by one of ordinary skill in the art and may vary depending on the type of gas turbine and load. A conventional device for measuring pressure can be used for measuring the pressure of HP drum 135 in HRSG 120. Conventional HRSG’s include systems for automatically monitoring HP drum pressure.

[0018] After a new pressure value (NP) has been measured and read, in step 210, it is compared with the sum of the last pressure value (PP) measured during the preceding time period and an offset (e.g., 0.69 bar (10 psi)). If the new pressure value (NP) is greater than the preceding pressure value (PP) plus the offset, then it is determined whether this is the first instance in which this condition has occurred (i.e., NP > PP + offset) in step 230. If this is the first instance, then the new pressure value (NP) becomes the temporary pressure setpoint (Ptemp) in step 240. If this is not the first instance that the new pressure value (NP) is greater than the preceding pressure value (PP) plus an offset, then the temporary pressure setpoint (Ptemp) is maintained in step 250. Once gas turbine 110 is loaded sufficiently and continues to increase its operating speed, the temporary pressure setpoint does not change since the drum pressure continues to rise and the temporary pressure setpoint (Ptemp) remains locked in step 250. As long as the previous pressure (PP) remains lower than the new pressure (NP), the pressure setpoint will remain locked.

[0019] Otherwise, if, in step 210, the preceding pressure value (PP) plus the offset is greater than or equal to the new pressure value (NP), the temporary pressure setpoint (Ptemp) becomes the new pressure value (NP) in step 220. When the previous pressure (PP) becomes the temporary pressure setpoint (Ptemp) in step 240, or is maintained in step 250 or the previous pressure (PP) becomes the temporary pressure setpoint (Ptemp) in step 220, the temporary pressure setpoint (Ptemp) is
compared with the floor pressure setpoint (Pfloor) in step 260. The floor pressure setpoint can vary and may be on the order of 49.6 bar (720 psi). If the temporary pressure setpoint (Ptemp) is greater than the floor pressure (Pfloor), then the pressure setpoint (Pset) becomes the temporary pressure setpoint (Ptemp) in step 270. Otherwise, the floor pressure setpoint (Pfloor) is set as the pressure setpoint (Pset) in step 280. In the next time step, the previous pressure (PP) is set as the new pressure (NP) in step 290 and control of the process then returns to step 205 to repeat the process for the next time period. In the next time period, another new pressure value (NP) is measured and the process is repeated.

[0020] Using the method shown in Fig. 2, the pressure setpoint is set so HP drum 135 is not de-pressurized when the pressure of HP drum 135 is greater than the floor pressure setpoint during the start-up procedure of advanced machine including the gas turbine 110. Therefore, the energy in HP drum 135 is conserved during the start-up procedure of the advanced machine including gas turbine 110, and time and energy is not wasted to rebuild pressure in HP drum 135 after HP drum 135 has been de-pressurized.

Claims

1. A method for controlling a flow of cooling steam in a power system, said power system including a gas turbine (110) connected to a heat recovery steam generator (120) including a drum (135), said method being characterized by the steps of:

   measuring pressure (NP) of said drum (135) during start-up of said power system; and

   setting a pressure setpoint (Pset) based on the measured pressure (NP) of the drum (135), said pressure setpoint (Pset) controlling at least one bypass valve (125) providing steam from said heat recovery steam generator (120) for cooling said gas turbine (110).

2. The method of claim 1, further comprising comparing a temporary pressure (Ptemp) based on the measured drum pressure (NP) to a floor pressure setpoint (Pfloor).

3. The method of claim 2, wherein said step of setting a pressure setpoint (Pset) further comprises, when said temporary pressure value (Ptemp) is greater than said floor pressure setpoint (Pfloor), setting said pressure setpoint (Pset) equal to said temporary pressure (Ptemp).

4. The method of claim 2, further comprising a step of, when said temporary pressure (Ptemp) is greater than said floor pressure setpoint (Pfloor), measuring the drum pressure (NP) until said gas turbine (110)

is fired or until one of the temporary pressures (Ptemp) based on the measured drum pressures (NP) is less than said floor pressure setpoint (Pfloor).

5. A system for generating power comprising:

   a gas turbine (110);
   a steam generator (120) including a drum (135) providing steam to said gas turbine (110); and
   at least one valve (125) controlling a flow of steam from said steam generator (120) to said gas turbine (110); characterized by

   a control system (140) configured to determine a sliding pressure setpoint and a pressure of said drum (135) and control said valve (125) to provide steam to said gas turbine (110) when a pressure (NP) of said drum (135) is greater than the pressure setpoint (Pset).

6. The system of claim 5, wherein said pressure setpoint (Pset) is determined by 1) measuring the pressure (NP) of said drum (135) during start-up of said system and 2) setting said pressure setpoint (Pset) based on the measured drum pressure (NP).

7. The system of claim 6, wherein when a temporary pressure (Ptemp) based on the measured drum pressure (NP) is greater than a floor pressure setpoint (Pfloor), said pressure setpoint (Pset) is set equal to the temporary pressure (Ptemp).

8. The system of claim 6, wherein when a temporary pressure (Ptemp) based on the measured drum pressure (NP) is greater than a floor pressure setpoint (Pfloor), the pressure (NP) of said drum (135) is continuously measured until one of 1) said gas turbine (110) is fired or 2) any one of the temporary pressures (Ptemp) based on the measured drum pressures (NP) is less than said floor pressure setpoint (Pfloor).

9. The system of claim 8, wherein when any one of the temporary pressures (Ptemp) is not greater than the floor pressure setpoint (Pfloor), said pressure setpoint (Pset) is set equal to said floor pressure setpoint (Pfloor).

10. The system of claim 6, wherein said at least one valve (125) includes at least one of a high pressure bypass valve (125) and an intermediate pressure bypass valve (125).

Patentansprüche

1. Verfahren zur Steuerung eines Kühl dampfstroms in einem Energieerzeugungssystem, wobei das Energieerzeugungssystem eine Gasturbine (110) ent-
hält, die mit einem eine Trommel (135) enthaltenden Wärmerückgewinnungsdampfgenerator (120) ver
bunden ist, wobei das Verfahren durch die Schritte gekennzeichnet ist:

1. Messen eines Druckes (NP) der Trommel (135) während des Hochfahrens des Energieerzeu-
gungssystems; und
2. Einstellen eines Druck-Sollwertes (Pset) auf der Basis des gemessenen Druckes (NP) der Trommel (135), wobei der Druck-Sollwert (Pset) wenigstens ein Bypassventil (125) steuert, das Dampf aus dem Wärmerückgewinnungsdampfgenerator (120) zum Kühl der Gasturbine (110) liefert.

2. Verfahren nach Anspruch 1, welches ferner den Vergleich eines temporären Drucks (Ptemp) auf der Basis des gemessenen Trommeldruckes (NP) mit einem Mindestdruck-Sollwert (Pfloor) aufweist.


4. Verfahren nach Anspruch 2, das ferner, wenn der temporäre Druck (Ptemp) größer als der Mindestdruck-Sollwert (Pfloor) ist, eine Messung des Trommeldruckes (NP) aufweist, bis die Gasturbine (110) gezündet wird oder bis einer von den temporären Drücken (Ptemp) auf der Basis der gemessenen Trommeldrücke (NP) kleiner als der Mindestdruck-Sollwert (Pfloor) ist.

5. System zum Erzeugen von Energie, aufweisend:

- eine Gasturbine (110);
- einen Dampfgenerator (120) mit einer Dampf an die Gasturbine (110) liefernden Trommel (135); und
- wenigstens ein Ventil (125), das einen Dampfstrom aus dem Dampfgenerator (120) zu der Gasturbine (110) steuert.

gekennzeichnet durch:

- ein Steuersystem (140), das so konfiguriert ist, dass es einen gleitenden Druck-Sollwert und einen Druck der Trommel (135) bestimmt und das Ventil (125) steuert, um Dampf an die Gasturbinne (110) zu liefern, wenn ein Druck (NP) der Trommel (135) größer als der Druck-Sollwert (Pset) ist.


7. System nach Anspruch 6, wobei, wenn ein temporärer Druckwert (Ptemp) auf der Basis des gemessenen Trommeldruckes (NP) größer als ein Mindestdruck-Sollwert (Pfloor) ist, der Druck-Sollwert (Pset) mit dem temporären Druck (Ptemp) gleichgesetzt wird.

8. System nach Anspruch 6, wobei, wenn ein temporärer Druck (Ptemp) auf der Basis des gemessenen Trommeldruckes (NP) größer als ein Mindestdruck-Sollwert (Pfloor) ist, der Druck-Sollwert (Pset) dem Mindestdruck-Sollwert (Pfloor) gleichgesetzt wird.


10. System nach Anspruch 6, wobei das wenigstens eine Ventil (125) wenigstens eines von einem Hochdruck-Bypassventil (125) und einem Zwischen-Druck-Bypassventil (125) enthält.

Reverdications

1. Procédé pour réguler un écoulement de vapeur de refroidissement dans un système de production d'énergie, ledit système de production d'énergie comprenant une turbine à gaz (110) reliée à un générateur (120) de vapeur à récupération de chaleur comprenant un tambour (135), ledit procédé étant caractérisé par les étapes consistant à:

- mesurer une pression (NP) dudit tambour (135) pendant le démarrage dudit système de production d'énergie ; et
- établir un point de consigne (Pset) de pression d’après la pression mesurée (NP) du tambour (135), ledit point de consigne (Pset) de pression commandant au moins un clapet de dérivation (125) fournissant de la vapeur issue dudit générateur (120) de vapeur à récupération de chaleur pour refroidir ladite turbine à gaz (110).

2. Procédé selon la revendication 1, comprenant en outre une étape consistant à comparer une valeur
de pression temporaire (P\text{temp}) reposant sur la pression (NP) mesurée dans le tambour, avec un point de consigne plancher (P\text{floor}) de pression.

3. Procédé selon la revendication 2, dans lequel ladite étape d’établissement d’un point de consigne (P\text{set}) de pression comprend en outre, lorsque ladite valeur de pression temporaire (P\text{temp}) est supérieure audit point de consigne plancher (P\text{floor}) de pression, l’étape consistant à établir ledit point de consigne (P\text{set}) de pression à la même valeur que ladite valeur de pression temporaire (P\text{temp}).

4. Procédé selon la revendication 2, comprenant en outre une étape consistant, lorsque ladite valeur de pression temporaire (P\text{temp}) est supérieure audit point de consigne (P\text{floor}) de pression, à mesurer la pression (NP) dans le tambour jusqu’à ce que ladite turbine à gaz (110) soit allumée ou jusqu’à ce qu’une des pressions temporaires (P\text{temp}) reposant sur les pressions mesurées (NP) dans le tambour soit inférieure audit point de consigne plancher (P\text{floor}) de pression.

5. Système pour produire de l’énergie, comprenant :

   - une turbine à gaz (110) ;
   - un générateur (120) de vapeur comprenant un tambour (135) fournissant de la vapeur à ladite turbine à gaz (110) ; et
   - au moins un clapet (125) régulant un écoulement de vapeur dudit générateur (120) de vapeur à ladite turbine à gaz (110) ; caractérisé par :

     - un système de commande (140) conçu pour déterminer un point de consigne glissant de pression et une pression dudit tambour (135) et pour commander ledit clapet (125) afin de fournir de la vapeur à ladite turbine à gaz (110) lorsqu’une pression (NP) dudit tambour (135) est supérieure au point de consigne (P\text{set}) de pression.

6. Système selon la revendication 5, dans lequel ledit point de consigne (P\text{set}) de pression est déterminé 1) en mesurant la pression (NP) dudit tambour (135) pendant le démarrage dudit système et 2) en établissant ledit point de consigne (P\text{set}) de pression d’après la pression mesurée (NP) dans le tambour.

7. Système selon la revendication 6, dans lequel, lorsqu’une pression temporaire (P\text{temp}) reposant sur la pression mesurée (NP) dans le tambour est supérieure à un point de consigne plancher (P\text{floor}) de pression, ledit point de consigne (P\text{set}) de pression est établi à la même valeur que la pression temporaire (P\text{temp}).