A METHOD OF JOINING SURFACES

VERFAHREN ZUM VERBINDEN VON OBERFLÄCHEN

PROCEDE D’ASSEMBLAGE DE SURFACES

Designated Contracting States:
AT DE FI SE

Priority:
06.04.1998 EP 98850049
06.04.1998 US 80833 P

Date of publication of application:
24.01.2001 Bulletin 2001/04

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EP-A- 0 493 010
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US-A- 3 929 695

PATENT ABSTRACTS OF JAPAN vol. 009, no.
233 (C-304), 19 September 1985 (1985-09-19) &
JP 60 090251 A (KIYUUSHIYUU TAIKA RENGA
KK), 21 May 1985 (1985-05-21)

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The present invention relates to a method of joining cellulosic fibre containing surfaces by means of a phenolic resin, phenol-resorcinol, or resorcinol resin based adhesive system whereby at least one of the surfaces is treated with a cure promoter composition prior to application of the adhesive system. It also relates to a cure promoter composition for a phenolic resin, phenol-resorcinol, or resorcinol resin based adhesive system.

A "cure promoter" is a substance, i.e. a compound or a composition, which increases the curing rate of an adhesive on forming of a joint. It should be distinguished from "hardeners" and "curing agents", which are substances used to initiate the curing process of an adhesive system.


Resorcinol resin and phenol-resorcinol resin adhesives can generally be cured at both low and elevated temperatures, whereas phenolic resin adhesives can generally only be cured at elevated temperatures, i.e. T ≥ 100 °C. The molar ratio of formaldehyde:phenol-resorcinol and formaldehyde:resorcinol (hereinafter both referred as HCHO:ArOH) is generally ≤ 0.80 for phenol-resorcinol and resorcinol resin adhesives, while the molar ratio of formaldehyde:phenol (hereinafter referred as HCHO:PhOH) for phenolic resin adhesives is generally ≥ 1.0.

By an "adhesive system" is herein meant a curing formulation of a resin and a hardener or a curing agent.

A "cellulosic fibre containing surface" may in the present context be a surface substantially defined by fibres of cellulose or one or more cellulosic substances, or combinations thereof. Examples of cellulosic fibre containing surfaces are the surfaces of wood based panels, paper or paperboard. The term "wood based panel" comprises, inter alia, plywood, particleboards, flakeboards, fibreboards, hardboards and medium density fibreboards (MDF). The present invention also covers embodiments in which only a thin surface stratum contains cellulosic fibres, the stratum being applied on the surface of an object of a basically non-cellulosic nature.

EP 493,010 discloses a method belonging to the general technical field indicated in the introduction. Pieces of unseasoned wood are joined by means of an adhesive formulation, whereby a cure promoter is brought into contact with the adhesive. Formaldehyde based adhesives are said to be preferred, and phenol and resorcinol are indicated as examples of components that may be used in such adhesives. Lewis and Bronsted acids are among the cure promoters mentioned specifically organic acids of low molecular weight. Basic chemicals (pH>7) which will react on contact with the adhesive to change the nature of a conventional adhesive to a fast curing adhesive are indicated to constitute a preferred class of cure promoters. Sodium periodate is also used in one of the examples.

These specific promoter chemicals indicated in EP 493,010 are all burdened by serious disadvantages, such as being poisonous, e.g. chromic acid, zinc salts, and aluminium salts, or giving rise to odour problems, e.g. ammonia, amines and amine derivatives, or both, e.g. formic acid and trichloroacetic acid. Sodium periodate is known to be a strong oxidising agent, giving rise to severe fire hazards.

It has also been found that when ammonia or an amine or an amine derivative is used as cure promoter the exact dosing of the promoter chemical is extremely critical; even at a minor overdose of the promoter the curing of the resin will be premature, as it will cure before it has penetrated the wood sufficiently to provide a durable joint between the surfaces.

The present invention accordingly provides a method of joining cellulosic fibre containing surfaces and a cure promoter composition suitable for use in the method, by which enhanced adhesive and strength properties are obtained and at the same time the above mentioned problems can be overcome.

The claimed method relates to joining of cellulosic fibre containing surfaces by means of a phenolic, phenol-resorcinol, or resorcinol resin based adhesive system, whereby at least one of the surfaces is treated with a cure promoter prior to the adhesive system being applied, in which method a cure promoter comprising a carbonate is used.

The claimed method also relates to a cure promoter composition for a phenolic, phenol-resorcinol, or resorcinol resin based adhesive system, wherein the cure promoter composition comprises a water soluble salt of carbonic acid, a water retaining and viscosity regulating agent and a base.

The surface treated with the cure promoter composition may, for instance, be the surface of a wood based panel or the surface of a paper or a paperboard. The wood based panel may for instance be a particleboard, flakeboard, hardboard, fibreboard, specifically a medium density fibreboard (MDF), or be made of plywood, although this listing is not exhaustive.

Suitable adhesive systems for use in the present invention are those based on phenolic, phenol-resorcinol, or resorcinol resins, and preferably those based on phenol-resorcinol, or resorcinol resins. The HCHO:ArOH molar ratio of the phenol-resorcinol and resorcinol resin component of the adhesive system is suitably 0.4:1 to 0.8:1, preferably 0.45:1 to 0.75:1 and most preferably 0.50:1 to 0.70:1. The resorcinol:phenol molar ratio of the phenol-resorcinol resin component of the adhesive system is suitably 1.0:1:1, preferably 9:1-0.15:1 and most preferably 7:1-0.25:1.
The adhesive systems used in the claimed method are cured at a temperature of suitably 10 to 100 °C, preferably 15 to 80 °C and most preferably at about room temperature, for instance at 20 to 40 °C.

The carbonate according to the method is preferably a water-soluble salt of carbonic acid, such as for instance Na₂CO₃, NaHCO₃, K₂CO₃, KHCO₃, (NH₄)₂CO₃, or NH₄HCO₃. The carbonate may also be a combination of two or more water-soluble carbonic acid salts. The cure promoter composition suitably comprises 0.5 - 45 weight percent water soluble carbonic acid salt, preferably 5 - 40 weight percent and most preferably 10 - 35 weight percent, based on the total weight of the cure promoter composition.

In one embodiment of the present method, the carbonate is 1,3-dioxolan-2-one (Chemical Abstracts Service Registry Number 96-49-1) or a higher homolog thereof, such as for instance 4-methyl-1,3-dioxolan-2-one (Chemical Abstracts Service Registry Number 108-32-7), or a combination thereof. The carbonate may also be a combination of 1,3-dioxolan-2-one, or a higher homolog thereof, and one and more water-soluble carbonic acid salts, for instance one or more of the salts indicated above.

Preferably, in the present method, the cure promoter composition additionally comprises a base, in particular an alkali. By "alkali" is meant water soluble hydroxides of alkali metals and alkaline earths, in particular Li, K, Na, Rb, Cs, and Ca. Preferably, the alkali is NaOH or KOH. The alkali is suitably used in an amount of up to about 30 percent by weight, based on the total weight of the cure promoter composition, preferably up to about 10 percent by weight and most preferably up to about 5 percent by weight.

Preferably, in the present method, the cure promoter composition additionally comprises a water retaining and viscosity regulating agent, such as for instance polyvinyl alcohol, hydroxy ethyl cellulose, carboxy methyl cellulose, ethylene glycol, polyethylene glycol, propylene glycol, polypropylene glycol, or a combination thereof.

Preferably, the present method, the cure promoter composition is substantially formaldehyde and/or resorcinol free and most preferably substantially resorcinol free.

Furthermore, the claimed cure promoter composition additionally comprises a water retaining and viscosity regulating agent, such as for instance polyvinyl alcohol, hydroxy ethyl cellulose, carboxy methyl cellulose, ethylene glycol, polyethylene glycol, propylene glycol, polypropylene glycol, or a combination thereof.

Preferably, the claimed cure promoter composition is substantially formaldehyde and/or resorcinol free and most preferably substantially resorcinol free.

The present invention is illustrated by means of some non-limiting examples below.

**EXAMPLES**

In these examples a thixotropic PRF adhesive system was used. The formaldehyde:resorcinol:phenol molar ratio of the PRF resin component of said system was 1.5:1.5:1.0. At 25 °C, said resin component had a pH of 8 and a solid content (measured after 3 h at 100 °C) of 57%. Viscosity value (Brookfield LVT sp4) at 3 rpm was 14 Pas, 5.6 Pas at 12 rpm, and 2.6 Pas at 60 rpm. The composition of the hardener used is given below in Table I, whereby the percentages are based on the total weight of the hardener:

<table>
<thead>
<tr>
<th>Table I</th>
</tr>
</thead>
<tbody>
<tr>
<td>Formaldehyde</td>
</tr>
<tr>
<td>Olive stone flour</td>
</tr>
<tr>
<td>Methanol</td>
</tr>
<tr>
<td>Thickener</td>
</tr>
<tr>
<td>Water</td>
</tr>
</tbody>
</table>
Example 1: In this example two different cure promoter compositions, A and B, formulated according to the present invention, were used. The compositions of the cure promoter compositions are given in Table II below.

<table>
<thead>
<tr>
<th>Component</th>
<th>weight-% based on the total weight of the cure promoter composition</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>cure promoter composition A</td>
</tr>
<tr>
<td>Water</td>
<td>85%</td>
</tr>
<tr>
<td>Sodium carbonate</td>
<td>12%</td>
</tr>
<tr>
<td>Sodium hydroxide (45% in water)</td>
<td>3%</td>
</tr>
</tbody>
</table>

In a first experiment two spruce wood blocks (32 x 5.5 x 2.0 cm), having a moisture ratio of 12%, were agglutinated. The surfaces to be joined were both treated with cure promoter composition A at an ambient temperature of 20°C. The amount of cure promoter composition used was 35 g/m² wood block surface. Directly after this treatment about 300 g/m² of the PRF adhesive was applied. The surfaces were pressed together for 40 minutes, at a temperature of 20°C and a relative humidity of 65%, with a pressure of 700 kPa. This experiment was repeated twice using the same experimental conditions, except that in the second experiment the surfaces were pressed together for 60 minutes, and in the third experiment for 90 minutes. After pressing the wood blocks were cut apart by means of a chisel, and the wood failure percentages were determined; these percentages are given in Table III below.

Example 2: The agglutinations in Example 1 were repeated, except that cure promoter composition B was used. After pressing the wood blocks were likewise cut apart by means of a chisel, and the wood failure percentages were determined; these percentages are given in Table III below.

Example 3: The agglutinations in Example 1 were repeated, except that no cure promoter composition was used, i.e. Example 3 is a reference example. After pressing the wood blocks were cut as in the previous examples, and the wood failure percentages were likewise determined. Again the obtained percentages are given in Table III below.

Example 4: Also in this experiment two spruce wood blocks (32 x 5.5 x 2.0 cm), having a moisture ratio of 12%, were agglutinated. However, only one of the surfaces to be joined was treated with cure promoter composition B at an ambient temperature of 20°C. The amount of cure promoter composition used was 60 g/m² wood block surface. Directly after this treatment about 200 g/m² of the PRF adhesive was applied. The surfaces were pressed together for 50 minutes, at a temperature of 20°C and a relative humidity of 65%, with a pressure of 700 kPa.

After this pressing operation the wood block assembly was sawn in two pieces, one of which was directly cut apart by means of a chisel, while the other one was cut apart twenty-four hours later, again by means of a chisel; the wood failure percentages were determined at each occasion; these percentages are given in Table V below.

Example 5: The agglutination in Example 4 was repeated, except that cure promoter composition C, formulated according to Table IV below, was used. After pressing the wood block was sawn and cut apart by means of a chisel as in Example 4, and the wood failure percentages were determined, and the obtained percentages are given in Table V below.

<table>
<thead>
<tr>
<th>Press time (minutes)</th>
<th>Press time 40 minutes</th>
<th>Press time 60 minutes</th>
<th>Press time 90 minutes</th>
</tr>
</thead>
<tbody>
<tr>
<td>Example 1</td>
<td>75%</td>
<td>70%</td>
<td>50%</td>
</tr>
<tr>
<td>Example 2</td>
<td>50%</td>
<td>90%</td>
<td>95%</td>
</tr>
<tr>
<td>Example 3</td>
<td>0%</td>
<td>5%</td>
<td>10%</td>
</tr>
</tbody>
</table>

A high percentage disrupted wood fibres indicates that the fracture appeared in the wood blocks rather in the adhesive joint, thus a higher percentage means better adhesion performance.

As can be seen from these examples the present cure promoter composition provides for excellent adhesion properties already at short press time.

Example 4: Also in this experiment two spruce wood blocks (32 x 5.5 x 2.0 cm), having a moisture ratio of 12%, were agglutinated. However, only one of the surfaces to be joined was treated with cure promoter composition B at an ambient temperature of 20°C. The amount of cure promoter composition used was 60 g/m² wood block surface. Directly after this treatment about 200 g/m² of the PRF adhesive was applied.

The surfaces were pressed together for 50 minutes, at a temperature of 20°C and a relative humidity of 65%, with a pressure of 700 kPa.

After this pressing operation the wood block assembly was sawn in two pieces, one of which was directly cut apart by means of a chisel, while the other one was cut apart twenty-four hours later, again by means of a chisel; the wood failure percentages were determined at each occasion; these percentages are given in Table V below.

Example 5: The agglutination in Example 4 was repeated, except that cure promoter composition C, formulated according to Table IV below, was used. After pressing the wood block was sawn and cut apart by means of a chisel as in Example 4, and the wood failure percentages were determined, and the obtained percentages are given in Table V below.
Example 6: The agglutination in Example 4 was repeated, except that no cure promoter composition was used. After pressing the wood block was sawn and cut apart by means of a chisel as in Example 4, and the wood failure percentages were determined, and the obtained percentages are given in Table V below.

<table>
<thead>
<tr>
<th>Table V</th>
</tr>
</thead>
<tbody>
<tr>
<td>After pressing for 50 minutes</td>
</tr>
<tr>
<td>Example 4</td>
</tr>
<tr>
<td>Example 5</td>
</tr>
<tr>
<td>Example 6</td>
</tr>
</tbody>
</table>

Example 7: In this experiment two spruce wood blocks (32 x 5.5 x 2.0 cm), having a moisture ratio of 12%, were agglutinated. The surfaces to be joined were both treated with cure promoter composition B at an ambient temperature of 20°C. The amount of cure promoter composition used was 60 g/m² wood block surface. Directly after this treatment about 200 g/m² of the PRF adhesive was applied. The surfaces were pressed together for 110 minutes, at a temperature of 20°C and a relative humidity of 65%, with a pressure of 700 kPa. This experiment was repeated twice. After pressing the wood blocks were cut apart by means of a chisel, and the wood failure percentages were determined; these percentages are given in Table VI below, labelled “Spruce I” and “Spruce II”.

Example 8: The experiments in Example 7 were repeated, except that the cure promoter was a 12.5 weight-% ammonia solution (cf. EP 493,010). After pressing the wood blocks were cut apart by means of a chisel, and the wood failure percentages were determined; these percentages are given in Table VI below, labelled “Spruce I”, “Spruce II”, “Pine I”, and “Pine II”.

Example 9: These experiments were repeated, the only exception being that pine wood blocks were used instead of spruce wood blocks. After pressing the wood blocks were cut apart by means of a chisel, and the wood failure percentages were determined; these percentages are given in Table VI below, labelled “Pine I” and “Pine II”.

Table VI

<table>
<thead>
<tr>
<th>Example 7</th>
<th>Spruce I</th>
<th>Spruce II</th>
<th>Pine I</th>
<th>Pine II</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>55%</td>
<td>30%</td>
<td>65%</td>
<td>65%</td>
</tr>
</tbody>
</table>

Evidently the present cure promoter composition provides for improved adhesion properties in relation to prior art cure promoters.

The foregoing describes the invention including preferred forms and examples thereof. Alternations and variations to the method and composition of the invention as will be apparent to those skilled in the art are intended to be incorporated in the scope hereof, as defined in the following claims.

Claims

1. A method of joining cellulosic fibre containing surfaces by means of a phenolic, phenol-resorcinol, or resorcinol
1. Verfahren zum Verbinden von Oberflächen, die Cellulosefasern enthalten, mittels eines auf einem Phenolharz,
einem Phenol-Resorcinharz oder einem Resorcinharz basierenden Haftsystems, wobei mindestens eine der Oberflächen vor der Aufbringung des Haftsystems mit einer die Här tung fördernden Zusammensetzung behandelt wird, dadurch gekennzeichnet, dass die die Här tung fördernde Zusammensetzung ein Carbonat umfasst.

2. Verfahren gemäß Anspruch 1, dadurch gekennzeichnet, dass das Carbonat ein wasserlösliches Salz der Kohlensäure ist.

3. Verfahren gemäß Anspruch 2, dadurch gekennzeichnet, dass das wasserlösliche Salz Na₂CO₃, NaHCO₃, K₂CO₃, KHCO₃, (NH₄)₂CO₃, NH₄HCO₃ oder ein Gemisch davon ist.

4. Verfahren gemäß Anspruch 1, dadurch gekennzeichnet, dass das Carbonat 1,3-Dioxolan-2-on oder ein höheres Homologes davon oder ein Gemisch davon ist.

5. Verfahren gemäß einem der Ansprüche 1 bis 4, dadurch gekennzeichnet, dass die die Här tung fördernde Zusammensetzung zusätzlich eine Base umfasst.

6. Verfahren gemäß Anspruch 5, dadurch gekennzeichnet, dass die Base ein Alkali ist.

7. Verfahren gemäß Anspruch 6, dadurch gekennzeichnet, dass die Menge der Base bis zu etwa 30 Gewichtsprozent beträgt, bezogen auf das Gesamtgewicht der die Här tung fördernden Zusammensetzung.

8. Verfahren gemäß einem der Ansprüche 1 bis 7, dadurch gekennzeichnet, dass das Haftsystem bei einer Temperatur von 15-80 °C gehärtet wird.

9. Verfahren gemäß einem der Ansprüche 1 bis 8, dadurch gekennzeichnet, dass das Haftsystem auf einem Phenol-Resorcinharz oder auf einem Resorcinharz basiert.

10. Verfahren gemäß einem der Ansprüche 1 bis 9, dadurch gekennzeichnet, dass die die Här tung fördernde Zusammensetzung im Wesentlichen frei von Resorcin ist.

11. Verfahren gemäß einem der Ansprüche 1 bis 10, dadurch gekennzeichnet, dass die Oberfläche, welche mit der die Här tung fördernden Zusammensetzung behandelt wird, eine Holzplattenoberfläche ist.

12. Verfahren gemäß einem der Ansprüche 1 bis 11, dadurch gekennzeichnet, dass die Oberfläche, welche mit der die Här tung fördernden Zusammensetzung behandelt wird, eine Papieroberfläche oder Kartonoberfläche ist.


14. Die Här tung fördernde Zusammensetzung gemäß Anspruch 13, dadurch gekennzeichnet, dass das wasserlösliche Salz Na₂CO₃, NaHCO₃, K₂CO₃, KHCO₃, (NH₄)₂CO₃, NH₄HCO₃ oder ein Gemisch davon ist.


17. Die Här tung fördernde Zusammensetzung gemäß Anspruch 16, dadurch gekennzeichnet, dass die Menge der Base bis zu etwa 30 Gewichtsprozent beträgt, bezogen auf das Gesamtgewicht der die Här tung fördernden Zusammensetzung.

Revendications

1. Procédé d'assemblage de surfaces contenant des fibres cellulosiques à l'aide d'un système d'adhésif à base de résine au phénol, au résorcinol ou au phénol/résorcinol, dans lequel procédé l'on traite au moins l'une des surfaces avec une composition d'accélérateur de durcissement avant d'y appliquer le système d'adhésif, caractérisé en ce que cette composition d'accélérateur de durcissement contient un carbonate.

2. Procédé conforme à la revendication 1, caractérisé en ce que le carbonate est un sel hydrosoluble de l'acide carbonique.

3. Procédé conforme à la revendication 2, caractérisé en ce que le sel hydrosoluble est Na$_2$CO$_3$, NaHCO$_3$, K$_2$CO$_3$, KHCO$_3$, (NH$_4$)$_2$CO$_3$ ou NH$_4$HCO$_3$, ou une combinaison de ces sels.

4. Procédé conforme à la revendication 1, caractérisé en ce que le carbonate est la 1,3-dioxolane-3-one ou l'un de ses homologues supérieurs, ou une combinaison de ces composés.

5. Procédé conforme à l'une des revendications 1 à 4, caractérisé en ce que la composition d'accélérateur de durcissement contient en outre une base.

6. Procédé conforme à la revendication 5, caractérisé en ce que la base est un alcali.

7. Procédé conforme à la revendication 6, caractérisé en ce que la quantité de base représente jusqu'environ 30 % du poids total de la composition d'accélérateur de durcissement.

8. Procédé conforme à l'une des revendications 1 à 7, caractérisé en ce que l'on fait durcir le système adhésif à une température de 15 à 80 °C.

9. Procédé conforme à l'une des revendications 1 à 8, caractérisé en ce que le système adhésif est à base d'une résine au phénol/résorcinol ou au résorcinol.

10. Procédé conforme à l'une des revendications 1 à 9, caractérisé en ce que la composition d'accélérateur de durcissement ne contient pratiquement pas de résorcinol.

11. Procédé conforme à l'une des revendications 1 à 10, caractérisé en ce que la surface traitée avec la composition d'accélérateur de durcissement est une surface d'un panneau à base de bois.

12. Procédé conforme à l'une des revendications 1 à 11, caractérisé en ce que la surface traitée avec la composition d'accélérateur de durcissement est une surface de papier ou de carton.

13. Composition d'accélérateur de durcissement pour système d'adhésif à base de résine au phénol, au résorcinol ou au phénol/résorcinol, caractérisée en ce qu'elle contient un sel hydrosoluble de l'acide carbonique, une base et un agent de rétention d'eau et de régulation de la viscosité.

14. Composition d'accélérateur de durcissement, conforme à la revendication 13, caractérisée en ce que le sel hydrosoluble est Na$_2$CO$_3$, NaHCO$_3$, K$_2$CO$_3$, KHCO$_3$, (NH$_4$)$_2$CO$_3$ ou NH$_4$HCO$_3$, ou une combinaison de ces sels.

15. Composition d'accélérateur de durcissement, conforme à la revendication 13 ou 14, caractérisée en ce qu'elle ne contient pratiquement pas de résorcinol.

16. Composition d'accélérateur de durcissement, conforme à la revendication 13 ou 15, caractérisée en ce que la base est un alcali.

17. Composition d'accélérateur de durcissement, conforme à la revendication 13, caractérisée en ce que la quantité de base représente jusqu'environ 30 % du poids total de la composition d'accélérateur de durcissement.

18. Composition d'accélérateur de durcissement, conforme à la revendication 13, caractérisée en ce que l'agent de rétention d'eau et de régulation de la viscosité est du poly(alcool vinylique), de l'hydroxyéthyl-cellulose, de la carboxyméthyl-cellulose, de l'éthylèneglycol, du polyéthylèneglycol, du propylèneglycol ou du polypropylèneglycol,
ou une combinaison de ces composés.